

## An Improvement of CMOS Voltage Reference

**Abstract.** This paper presents a CMOS voltage reference design, which is widely used in electronic circuits, both analog and digital circuits. In the conventional, a CMOS voltage reference circuit design composed of several MOS transistors and complicated circuits, the output voltage cannot be adjusted to any levels. Therefore, in this paper proposed the CMOS voltage reference circuit design technique based on current combination circuit, which it was reduced number of MOS transistors and the proposed circuit is able to operate without complex startup circuit. The performance of the proposed circuit is confirmed through PSPICE simulation results, the circuit can be operated with supply voltage varies from 1.85 - 4 V, the output voltage reference is about  $500 \pm 2.5$  mV at wide temperature range of  $-58^\circ\text{C}$  to  $120^\circ\text{C}$ , it has very low temperature coefficient of about  $61.19$  ppm/ $^\circ\text{C}$ , and low power dissipation is  $5.51$   $\mu\text{W}$ .

**Streszczenie.** W artykule opisano ulepszone źródło napięcia wzorcowego w technologii CMOS. W ulepszonej technologii wykorzystuje się siemniej tranzystorów a możliwość ustawiania napięcia jest bardziej uniwersalna niż w typowych układach tego typu. (Ulepszone źródło napięcia wzorcowego w technologii CMOS)

**Keywords:** Temperature compensation, CMOS, Voltage reference, Weak inversion.

**Słowa kluczowe:** in the case of foreign Authors in this line the Editor inserts Polish translation of keywords.

### Introduction

The voltage reference circuit was developed and widely applied to electronic circuits which the stable power supply voltage requirement for proper circuit operations such as A/D and D/A converter, DRAM Flash memories, PLLs and others[1-3]. The low-power and low-voltage operations are widely used for portable devices, biomedical sensor and also included shopping intelligence tool in superstore [4-6]. The output voltage of generators are designed with low sensitivity to temperature, fabrication process and power supply variations. The CMOS voltage reference is one of generator circuit that can successfully achieve these requirements [7-9]. In the last few years, many researchers have reported the current and voltage reference circuit design technique to achieve the low temperature sensitivity and supply voltage variations [10-14]. However, conventional implementation of these circuits still composed of several MOS transistors and resistors for generating the bias current. Moreover, the above mentioned circuits are very complex and consumes a large chip area and power consumption [5-15].

Therefore, in this paper presents the CMOS voltage reference circuit design based on the new current summation technique that have opposite temperature coefficient for reference voltage generation which stabilized over process, supply voltage and temperature variations and proposed circuit is able to operate without complex startup circuit which this technique was reduced number of MOS transistors and providing an accurate voltage reference for low supply voltage operations.

### Principle of voltage reference circuit

The working principle of a voltage reference propose two parts of the circuit as shown in Fig.1. The first circuit is generated the voltage with a negative temperature coefficient of about  $-2$  mV/ $^\circ\text{C}$ , is called complementary to absolute temperature ( $V_{CTAT}$ ) and the other circuit is generated the voltage with a positive temperature coefficient of about  $0.086$  mV/ $^\circ\text{C}$ , is multiplied by gain  $K$  which has proportional to absolute temperature( $V_{PTAT}$ ).

The reference voltage generator is summed of CTAT and PTAT currents to generate a reference current ( $I_{ref}$ )

which is employed for generating the reference voltage ( $V_{ref}$ ), can be expressed as

$$(1) \quad V_{ref} = (I_{CTAT} + KI_{PTAT})R_{ref}$$

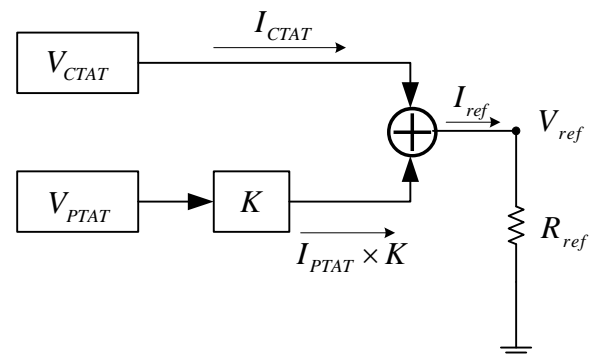


Fig.1. block diagram of a voltage reference circuit

The temperature compensation for reference voltage, the following condition must be achieved a zero-temperature coefficient [3, 8].

$$(2) \quad \frac{\partial V_{ref}}{\partial T} = 0$$

The voltage reference with a temperature coefficient ( $TC$ ) is formed by the min/max limits for the nominal output voltage over the operating temperature range is defined as follows.

$$(3) \quad TC = \frac{1}{V_{atroomtemp}} \left[ \frac{V_{max} - V_{min}}{T_{max} - T_{min}} \right] \cdot 10^6 \text{ ppm}/^\circ\text{C}$$

The voltage reference circuit exhibits a  $TC$  limit typically between  $20$  to  $100$  ppm/ $^\circ\text{C}$  [16].

### Purposed CMOS Voltage Reference circuit

The circuit configuration of CMOS voltage reference is shown in Fig. 2 can be divided into three parts. The first part is composed of transistors  $M1$ ,  $M3$  and  $R1$  for generating the current with negative temperature coefficient ( $I_{CTAT}$ ), second part is composed of transistors  $M2$  and  $R2$  for generating the current with a positive temperature

coefficient ( $I_{PTAT}$ ) and the last part is current mirror circuit which is consisted of transistors  $M4$ ,  $M5$  and  $M6$ . The  $M4$  is defined for summing the current of  $I_{CTAT}$  and  $I_{PTAT}$  which is independent of temperature and mirrored to the  $M6$  for generating the voltage reference ( $V_{ref}$ ).

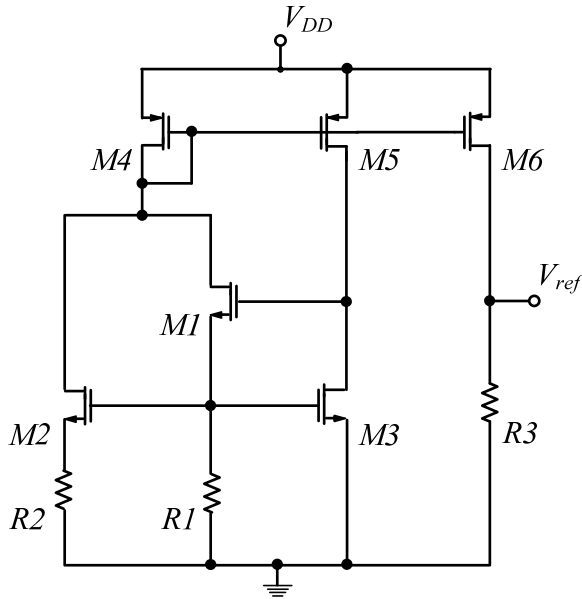


Fig.2. Proposed Voltage Reference Circuit

In the first part, the  $M1$  and  $M3$  are defined to operate in saturation and weak inversion region, respectively. Then, the drain current of  $M1$  and the gate-source voltage of  $M3$  ( $V_{gsM3}$ ) is given by

$$(4) \quad I_{D_{M1}} = \frac{1}{2} m_p C_{ox} \frac{W}{L} (V_{GS} - V_{th})^2$$

$$(5) \quad V_{gsM3} = nV_T \ln \left[ \frac{I_{ds3} \cdot L_3}{I_t \cdot W_3} \right] + V_{th}$$

Where  $V_T$  is the thermal voltage, can be written as

$$(6) \quad V_T = \frac{kT}{q}$$

Where  $k$  is the Boltzmann's constant ( $1.38 \times 10^{-23}$  J/K),  $q$  is electric charge ( $1.6 \times 10^{-19}$  C) and  $T$  is absolute temperature. The drain current of  $M3$  is expressed in term of exponential can be expressed as

$$(7) \quad I_{ds3} = I_t \frac{W_3}{L_3} e^{\frac{q(V_{gsM3} - V_{th})}{nkT}}$$

Where  $V_{th}$  is the threshold voltage,  $W_3$  and  $L_3$  is channel width and channel length of MOS transistor, respectively.

$$(8) \quad I_t = 2nm_n C_{ox} \left( \frac{kT}{q} \right)^2$$

Where  $I_t$  is the saturation current of the MOS transistor,  $n$  is the slope factor,  $C_{ox}$  is the gate oxide capacitance per unit area and  $\mu$  is the electron mobility,

Substituting equation (6), (7) and (8) into (5), then differentiation can be written as

$$(9) \quad \frac{\partial V_{gsM3}}{\partial T} = \frac{V_{gsM3}}{T} - 2n \frac{k}{q}$$

From eq. (9) found that, when increasing temperature the  $V_{gs}$  of MOS transistor  $M3$  will be decreased which is called  $V_{CTAT}$  and the  $I_{CTAT}$  is expressed by.

$$(10) \quad I_{CTAT} = \frac{V_{gsM3}}{R1}$$

In the second part, from the circuit as shown in fig. 2 the  $M2$  is defined to operate in weak inversion region and  $V_{R1}$  is equaled to  $V_{GS2} + V_{R2}$ . So the voltage drop across  $R2$  can be written as

$$(11) \quad V_{R2} = nV_T \ln m$$

Where  $m$  is aspect ratio of MOS transistors  $M2$  and  $M3$ , and  $I_{R2}$  is proportional to  $V_T$ , can be written as

$$(12) \quad I_{PTAT} = I_{R2} = \frac{nkT}{R2q} \ln m$$

From equation (12), found that the current  $I_{R2}$  has a positive temperature coefficient; it's clearly seen that when increasing temperature, the current  $I_{R2}$  will be increased.

In the last part, the current mirror circuit is composed of transistors  $M4$ ,  $M5$  and  $M6$ . The MOS transistor  $M4$  is defined for summing the current of  $I_{CTAT}$  and  $I_{PTAT}$  which is independent of temperature, can be expressed as

$$(13) \quad I_{ref} = I_{CTAT} + I_{PTAT}$$

By substituting (10) and (12) into (13) can be obtained

$$(14) \quad I_{ref} = \frac{V_{gsM3}}{R1} + \frac{nV_T}{R2} \ln m$$

The current  $I_{ref}$  is mirrored from  $M4$  to  $M6$ , then the reference voltage can be obtained as follow.

$$(15) \quad V_{ref} = I_{ref} R3$$

The output reference voltage can be achieved the low temperature coefficient and set at any level by changing the resistance value of  $R3$ .

Table 1. The parameters of transistors and resistors

Transistors	W/L(μm/μm)
$M1$	10 / 5
$M2$ - $M3$	50 / 5
$M4$ - $M5$	5 / 5
$M6$	10 / 5
Aspect Ration $M2/M3$	15/1
Resistors	( $K\Omega$ )
$R1$	1400
$R2$	230
$R3$	544

## Simulation results

The simulation results of the proposed voltage reference circuit are verified by PSPICE in a 0.5  $\mu\text{m}$  standard CMOS technology. The device parameters of MOS transistors and the resistors are shown in Table 1, Fig.2. shows the output reference voltage of about 500 mV under temperature variations from  $-58^\circ\text{C}$  to  $120^\circ\text{C}$  and voltage variation less than 2.5 mV, the temperature coefficient is 61.19 ppm/ $^\circ\text{C}$  and the power dissipation is only 5.51  $\mu\text{W}$  at the supply voltage  $V_{DD} = 2.0\text{ V}$ .

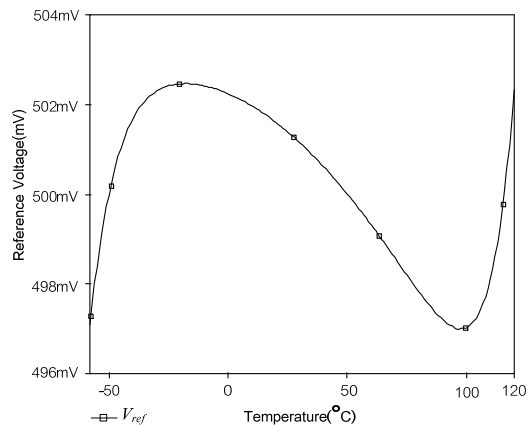


Fig.2. Temperature independence of the voltage reference

Fig.3. shows the currents  $I_{CTAT}$  and  $I_{PTAT}$  which has negative and positive temperature coefficient, respectively, after that both currents will be summed by  $M4$ , then mirrored to  $M6$  to produce  $I_{ref}$  and flow through a resistor ( $R3$ ) to create the  $V_{ref}$ .

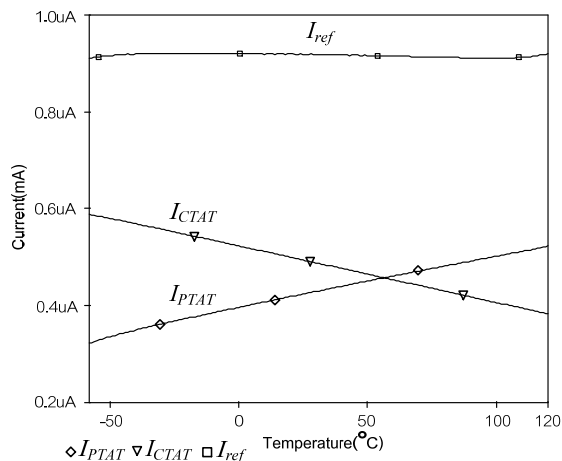


Fig.3. The currents  $I_{CTAT}$ ,  $I_{PTAT}$  and  $I_{ref}$  as function of temperature

Fig.4. shows the reference voltage as a function of supply voltage, which can be successfully operated from 1.85 V to 4.0 V, the reference voltage is set of about 500 mV and voltage variation is about 2.5 mV/V. at room temperature.

As shown in Fig. 5, the reference voltage dependence of the supply voltage range is changed from 2.0 to 3.5 V and different temperatures ( $-30$ ,  $30$  and  $120^\circ\text{C}$ ), the line regulation of the reference voltage is about 3.0 mV/V at room temperature.

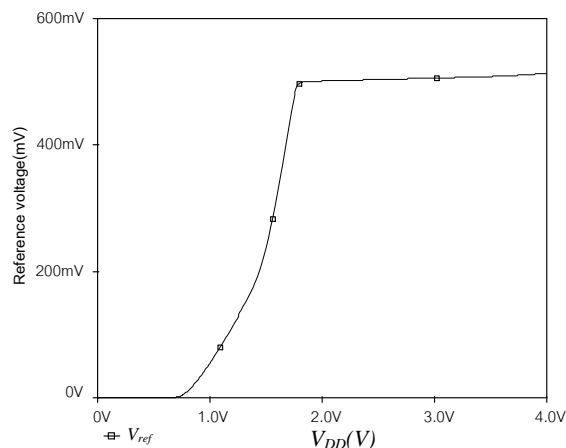


Fig.4. Reference voltage as a function of supply voltage

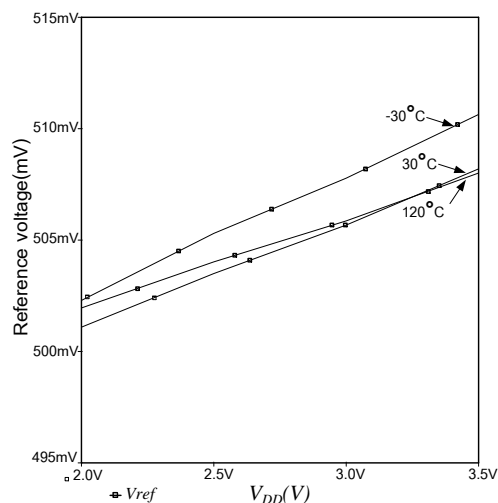


Fig.5. Reference voltage versus supply voltage variations and under different temperatures

## Conclusion

An improvement of CMOS voltage reference circuit with new technique for current combination circuit which has negative and positive temperature coefficient without startup circuit, this methodology can be reduced the number of MOS transistors, chip area and low power consumption.

The results of simulation for the proposed circuit is shown that the reference voltage is very stable for a wide range of temperature and supply voltage variations.

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